# Microscale Gas breakdown voltage dependence on electrode surface

Russell S. Brayfield, II, Andrew J. Fairbanks, Amanda M. Loveless, Shengjie Gao, Weihang Li, Caleb Darr, Jacqueline R. Malayter, Wenzhuo Wu, and Allen L. Garner\*

> Purdue University West Lafayette, IN 47907 [\\*algarner@purdue.edu](mailto:*algarner@purdue.edu)

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<sup>ci</sup>ence & Tec



# Motivation: Applications

- Induce breakdown
	- Combustion[1]
	- Electric micropropulsion[2]
	- Medicine<sup>[3]</sup>
- Prevent breakdown
	- For electric pulse applications[4]
	- Microelectromechanical systems (MEMS) are used in biotechnology, medicine, and communications[5]

[1] Y. Ju and W. Sun, "Plasma assisted combustion: Dynamics and chemistry," *Prog. Energy Combust. Sci.*, vol. 48, no. C, pp. 21–83, 2015. [2] W. P. Wright and P. Ferrer, "Electric micropropulsion systems," *Prog. Aerosp. Sci.*, vol. 74, pp. 48–61, Apr. 2015. [3] M. Martinez-Sanchez and J. E. Pollard, "Spacecraft Electric Propulsion-An Overview," *J. Propuls. Power*, vol. 14, no. 5, pp. 688–699, Sep. 1998. [4] A. L. Garner, A. Caiafa, Y. Jiang, S. Klopman, C. Morton, A. S. Torres, A. M. Loveless, and V. B. Neculaes, "Experimental Validation of a Compact, Flexible Pulsed Power Architecture for Ex Vivo Platelet Activation," PLoS ONE, vol. 12(7), 2017, Art. No. e0181214. [5] R. Bogue, "MEMS sensors: past, present and future," *Sens. Rev.*, vol. 27, no. 1, pp. 7–13, Jan. 2007. [6] H. G. Craighead, "Nanoelectromechanical Systems," *Science (80-. ).*, vol. 290, no. 5496, pp. 1532–1535, Nov. 2000.

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# Experimental Setup

- Tungsten dissection needles
	- 1 μm tip (Roboz Surgical Instrument Co., RS-6065)
- Copper plate cut to 12.7 mm<sup>2</sup>
- Two 1 MΩ resistors
	- Current limiting
	- Current viewing shunt
- DC high voltage supply (Stanford Research System, PS365, 10 kV)
- Two 100:1 voltage probes were connected across pin-plate connection and shunt resistor
- LeCroy Oscilloscope to record voltage and current at breakdown

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R. S. Brayfield, II, A. J. Fairbanks, A. M. Loveless, S. Gao, A. Dhanabal, W. Li, C. Darr, W. Wu, and A. L. Garner, "The impact of cathode surface roughness and multiple breakdown events on microscale gas breakdown at atmospheric pressure," J. Appl. Phys., vol. 125, 2019, Art. no. 203302.





# Experimental Design

- Copper plate surface modification
	- Wet polishing station with 400, 800, and 1200 grit polishing pads (Pace Technologies)
	- After polish the samples were soaked in acetone
- Plate surface divided into 2 regions
	- 1 breakdown event
	- 10 breakdown events
- AFM conducted pre-test
	- Initial surface roughness
	- Contamination
- Gaps distance set
	- Applied 35V and shorted gap
	- 1, 5, and 10  $\mu$ m
- Voltage slowly increased (~3V/s) until breakdown occurred
	- Current across gap observed on oscilloscope
- Measure voltage and current at which gap broke down

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#### Results: Pre-test AFM results





- 3 different surface modifications conducted
- RMS values show each surface has a different overall roughness
- Gives baseline for any change due to the discharge event during testing

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## Results: Observed Ablation

#### • Ablated craters observed after test

• Too deep to use AFM, so optical estimation was made







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#### Results: VI data



- Recorded for each test run
- Used current to act as indicator of breakdown

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# Results: Breakdown Voltage

- (a) 400 grit (b) 800 grit and (c) 1200 grit
- Clear increasing trend with number of breakdown events
- Breakdown events after the fifth event yield a statistically significant breakdown voltage between the 1  $\mu$ m gap and the other gap distance
- Behavior arises because the breakdown events alter the electrode surface, which contributes to the increased variation after multiple

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#### Results: Altered Breakdown Voltage



- Larger gap did not always result in higher breakdown voltage
- Crater significantly impacted required breakdown voltage

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## Results: Effective Gap Distance



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#### Results: Data vs. Model

• Fit to experimental data using breakdown model given by [1]

$$
\frac{\exp\left[\bar{\phi}^{3/2}/(\beta \bar{E})\right]}{\beta \bar{\phi}^{1/2} \exp\left(\bar{\phi}^{-1/2}\right)} \sqrt{\bar{p} \bar{d}_{eff}^2} \frac{\left\{1 - \gamma_{SE} \left[\exp\left(\bar{\alpha} \bar{d}_{eff}\right) - 1\right]\right\}}{\exp\left(\bar{\alpha} \bar{d}_{eff}\right) - 1}
$$
\n
$$
= \exp(1)(1 + 2\bar{E}),
$$

where  $\bar{d}_{eff}$  is the nondimensionalized gap distance plus the crater depth

• Also consider analytic limit given by [2]

$$
V = \left(E_*L\,\bar{d}_{eff}/\Lambda_2\right)\left[-\Delta_2 - \left(\Delta_2^2 - 2\Lambda_2\bar{\phi}^{3/2}/\beta\right)^{1/2}\right],
$$

Where  $\Delta_2 = -[\bar{\mu} + \bar{\nu}]$  and  $\bar{\mu} = \ln(\Lambda_2)/2 + \ln(\beta \bar{\phi}^{1/2}) +$  $\bar{\phi}^{-1/2} + 3/2$  and  $\bar{v} = \ln \{ \exp[\bar{p} \bar{d}_{eff} \exp(-1)] - 1 \} - \ln \{ 1 - \frac{1}{2} \}$  $\gamma_{SE} \left[ \exp(\bar{p}\bar{d}_{eff} \exp(-1)) \right] \right\} - \ln \left| \bar{T} \bar{p}^{-1} \bar{d}_{eff} \right|^{-2} \left| \bar{p} \right|$  $\binom{-2}{1}$  z represent the field emission and Townsend contributions, respectively, and  $\Lambda_2 = 10^{-5}$  is a fitting parameter



[1] A.M. Loveless and A.L. Garner, Phys. Plasmas, vol. 24, 2017, Art. no. 113522.

[2] G. Meng, X. Gao, A.M. Loveless, C. Dong, D. Zhang, K. Wang, B. Zhu, Y. Cheng, and A.L. Garner, Phys. Plasmas, vol. 25, 2018, Art. no. 082116.



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## Results: Data vs. Model

- (1): Numerical solution
- (2): Analytic solution
- (1) and (2) differ by  $^{\sim}10\%$  until the largest gap distances
- At largest gap distances,  $\bar{\alpha}\bar{d}_{eff} > 18$  – Meek's criterion for streamer discharge
	- Can we get streamers at microscale?





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### Results: Data vs. Model

- Each pair of symbols shows the product of ionization coefficient and gap distance after the 1st breakdown event and the 10<sup>th</sup> breakdown event.
- Crater formation alone can push breakdown behavior into the Paschen law regime even at the 1 and 5  $\mu$ m initial gap distances.

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#### Surface Roughness on  $\varphi$

- For large bumps (big flat region, or  $t = \tau/x$  << 1), the  $\varphi_{s}$  approaches a constant.
- For other periodicity, we can determine the effective  $\varphi_s$



**SKP** Tip

 $\overline{a}$ 

 $h_0 = a + d_0$ 

x<sub>o</sub> (scan step)

 $d_0 \sin(2\pi x/\tau)$ 

#### Future Work

- Assess the impact of aspect ratio on field enhancement  $\beta$  using designed nanoscale electrodes at atmospheric pressure, pressure, and sub-microscale gap distances.
- Continue exploring the impact of surface roughness on breakdown, particularly post-breakdown work function  $\phi$ .
- Incorporate  $\beta$  and  $\phi$  into the theory and compare to experiment.

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#### BACKUP



# Future Work: Surface Roughness Also Effects Work Function

- Geometry for measuring work function of a rough surface.
- Derive change in work function as a function of the capacitance of each increment of motion of the Kelvin Probe tip.
- Provides insight into the effect of surface roughness on measured work function that may be relevant since the geometry is similar to pin-to-plate.



Model adapted from Y. Wan, Y. Li, Q. Wang, K. Zhang, and Y. Wu, "The relationship of surface roughness and work function of pure silver by numerical modeling," Int. J. Electrochem. Sci., vol. 7, pp. 5204-5216, 2012.

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## Definitions From This Setup

Work function of a surface (where *V<sup>c</sup>* is contact potential difference) :

$$
\varphi_s = \varphi_{tip} - eV_c
$$

Equation for capacitance: 
$$
C_k = \int dC_k = \int_{n_0x}^{(n_0+1)x} \frac{\varepsilon_0 y_0 dx}{h_0 - d_0 \sin x} = \varepsilon_0 y_0 \int_{n_0x}^{(n_0+1)x} \frac{dx}{h_0 - d_0 \sin x}
$$
  
\n $R_q$  (surface roughness)  $R_q = d_0/\sqrt{2}$ 

SKP Tip Charge:  $c_{k0}(\varphi_t^0 - \varphi_s^0)$  $\frac{\partial_t^0 - \varphi_s^0}{\partial e} = \frac{\varepsilon_0 A(\varphi_t^0 - \varphi_s^0)}{\partial e}$ ea (where *A* is the scan tip area) Charge per scan area:  $Q = \frac{Q'S}{A}$  $\frac{\rho's}{A} = \frac{\varepsilon_0 x_0 y_0 (\varphi_t^0 - \varphi_s^0)}{ea}$  $\frac{(\Psi_t - \Psi_s)}{ea}$  (where  $x_0$  and  $y_0$  are the step sizes)

Change in WF per scan:

$$
\varphi_{s} = \varphi_{t} - \frac{eQ}{c_{k}} = \varphi_{t} - e \frac{\varepsilon_{0} x_{0} y_{0} (\varphi_{t}^{0} - \varphi_{s}^{0})}{ea} 1 / \left[ \varepsilon_{0} y_{0} \int_{n_{0} x}^{(n_{0} + 1)x} \frac{dx}{h_{0} - d_{0} \sin(\frac{2\pi x}{\tau})} \right]
$$



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# Derived Relationships and Asymptotic Behavior of Work Function

Change in WF over the entire scan area (average of all of the steps of the SKP):

$$
= \frac{1}{m} \left( \sum_{n=0}^{n=m-1} \varphi_t - e^{-\frac{\mathcal{E}_0 x_0 y_0 (\varphi_t^0 - \varphi_s^0)}{ea}} \frac{1}{\left| \varepsilon_0 y_0 \int_{n_0 x}^{(n_0+1)x} \frac{dx}{h_0 - d_0 \sin\left(\frac{2\pi x}{\tau}\right)} \right|},
$$

where  $m$  is the total number of scan steps



For large  $\tau$  (step size much smaller than surface roughness), we apply the small angle theory (tan*x* ≈ *x*) and use L'Hopital's rule to obtain

$$
\varphi_s \approx \frac{h_0}{\pi \sqrt{h_0^2 - d_0^2}} \qquad \qquad \varphi_{s, Ave} = \overline{\varphi_t^0} - \frac{(\overline{\varphi_t^0} - 1)}{a}
$$



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 $h<sub>0</sub>$ 

)

]

## Surface Roughness Periodicity on Surface Work **Function**



- For large bumps (big flat region, or  $t = \tau/x \ll 1$ ), the  $\varphi_s$  approaches a constant.
- For other periodicity, we can determine the effective  $\varphi_s$
- May allow fine-control of surface and full incorporation of surface effects into breakdown theory.

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#### Results: Tukey Test



- Breakdown events after the fifth event yield a statistically significant breakdown voltage between the 1  $\mu$ m gap and the other gap distance
- Behavior arises because the breakdown events alter the electrode surface, which contributes to the increased variation after multiple events

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